

DATASET OF THE REFRIGERATOR CASE
DESIGN OF CLOSED LOOP SUPPLY CHAINS : A PRODUCTION AND RETURN
NETWORK FOR REFRIGERATORS
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BIBLIOGRAPHIC DATA AND CLASSIFICATIONS		
Abstract	This paper contains the dataset for the refrigerator case concerning the design of a production and return network for refrigerators. Section 1 emphasises the major changes to the problem structure and assumptions used by Umeda et al. (1999). Section 2 contains the parameter settings. Section 3 contains the distance matrix for all locations.	
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Dataset of the refrigerator case

Design of closed loop supply chains: A production and return network for refrigerators

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Abstract

This paper contains the dataset for the refrigerator case concerning the design of a production and return network for refrigerators. Section 1 emphasises the major changes to the problem structure and assumptions used by Umeda et al. (1999). Section 2 contains the parameter settings. Section 3 contains the distance matrix for all locations.

Keywords: supply chain management, product design, network design, facility location, environment

1. Assumptions in the refrigerator case

Changes and additions compared to the original problem (Umeda et al., 1999):

- Thermal is open loop and therefore a sink and not a supply chain process
- Maintenance by the consumer is replaced by professional repair, after which the refrigerator is returned to the warehouse for sale. No modules or components are discarded after repair. There is a repair fee, that varies with the product type.
- Product designs (modular structure) are now input of the model instead of output of the model.
- Since all product designs are assumed to be equal in quality, their return quality is also assumed to be the same.
- Finished products are also sent to the warehouse before sale
- The volume unit used is always kilogram
- Module and product assembly are separate processes, product and module inspection and disassembly as well as product, module and component warehousing are one process and hence can be performed at one facility.
- The purchase price of components (see table 2 in Umeda et al., 1999) is left out since this is the price consumers pay when they purchase a part for maintenance or repair (themselves).
- Facility costs are assumed to be 50% fixed and 50% variable.
- Quality parameters have been set by the authors.
- In module rebuild (p8), non reusable components (see Table 2 Umeda et al., 1999) are replaced, the others are assumed to be functioning since the module as a whole has passed the inspection (p7). In other words, there are no faulty components among the 'reusable' ones. Components replaced in the module rebuild process (p8) are assumed to be scrapped locally at zero cost and neutral environmental impact.
- Due to some round offs and randomising, parameter settings may in general slightly differ from (Umeda et al., 1999)
- It is assumed that energy recycling produces no by-products except energy.
- There is no time dimension in this model, hence multiple reuse is impossible. Also, aspects like MTBF are not taken into account.
- WRER and MRER are not used in this case.
- 1 Kwh = $3.6 * 10^6$ Joule
- 1 yen = 1 euro cent

2. Parameter settings of the refrigerator case

The environmental optimisation criteria are e_1 (energy) and e_2 (waste volume).

The demand of finished product at the customer locations is $V_c = 91.000$ kg, divided over $c=c_1..c_{10}$, i.e. at each c there is a demand for a 1000 refrigerators of 91 kgs each.

The maximal volume of the external secondary market d , $V_d = \text{infinite}$ for $d=d_1..d_{10}$

The supply locations $s=s_1..s_{10}$, are Amsterdam, Athens, Barcelona, Belgrado, Berlin, Bern, Birmingham, Bologna, Bratislava, Nagasaki.

The customer locations $c=c_1..c_{10}$ are Manchester, Zaragoza, Milan, Munich, Hannover, Nuremberg, Oslo, Palermo, Paris, Prague.

The potential facility locations $f=f_1..f_{20}$, are Tokyo, Brussels, Budapest, Bukarest, Cologne, Copenhagen, Dresden, Dublin, Frankfurt, Genova, Hamburg, Naples, Helsinki, Krakow, Nagano, Lisbon, Lodz, London, Lyon, Madrid.

The thermal recycling locations $d=d_1..d_5$ are Rome, Sevilla, Sofia, Stockholm, Stuttgart.

The disposal locations $d=d_6..d_{10}$ are Turin, Valencia, Vienna, Warswa, Marseille.

The distance matrix between the 50 locations is available on request as DISTANCE50.XLS.

The supply chain processes are $p=p_1..p_9$. For each process the possible facility locations are given in $F(p)$.

P	Process description	F(p)
p1	Component manufacturing	f1, f15
p2	Warehousing	f2, f3, f11, f20
p3	Module assembly	f12, f16, f18
p4	Product assembly	f2, f3, f5, f8, f13, f14, f20
p5	Repair (maintenance)	f17, f19
p6	Disassembly	f6, f8, f14
p7	Inspection	f6, f8, f14
p8	Module rebuilt	f4, f9
p9	Material recycling	f7, f10

Section 2.1 contains the parameter settings of the components and the modules. Section 2.2 contains identity changes from material to component and from component to module for the forward chain and Section 2.3 contains the identity changes in the return part. Finally, Section 2.4 contains the cost parameters.

2.1 Components and modules

The components are a=a1..a25

Component	Description	Component	Description
a1	cabinet frame	a14	Base
a2	cabinet	a15	door 1
a3	cabinet pipe	a16	door 2
a4	duct in room	a17	door 3
a5	fan motor	a18	door 4
a6	evaporator case	a19	Gasket
a7	accumulator	a20	door plas.
a8	evaporator	a21	Spcb
a9	back grill	a22	mpcb
a10	compressor	a23	heater
a11	sideboard	a24	Tank
a12	radiator	a25	Dryer
a13	duct		

The modules are t=t1..t13

T	module weight+description	Components
t1	79.1 kg 'reuse-1'	base, sideboard, compressor, duct, accumulator, mpcb, spcb, radiator, evacover, ductin room, pipeincabinet, glassheater, tankassembly, dryer, fanmotor, cabinet, evaporator, backgrill, cabinetframe, door 4
t2	11.9 kg 'reuse-2'	door 1, door 2, door 3, door plas, gasket
t3	3.6 kg 'maint-1'	spcb, fanmotor
t4	0.4 kg 'maint-2'	dryer, pipeln cabinet
t5	0.6 kg 'maint-3'	glassheater, evaporator
t6	2.2 kg 'maint-4'	base, backgrill
t7	25.4 kg 'maint-5'	cabinet frame, door 3
t8	6.8 kg 'maint-6'	door plas, gasket
t9	2.6 kg 'pmpp-1'	mpcb, ductin room
t10	30.7 kg 'pmpp-2'	tank assembly, cabinet
t11	0.6 kg 'pmpp-3'	dryer, evaporator
t12	49.7 kg 'pmpp-4'	base, duct, radiator, cabinet frame, door 1, door 2, door 3, door 4, door plas, compressor
t13	3.7 kg 'pmpp-5'	sideboard, accumulator, evacover, glassheater, fanmotor, backgrill

The product designs are o= o1 (reuse type), o2 (maintenance type), o3 (pmpp type)

The materials are m= m1(Fe), m2 (plastics), m3(Cu), m4 (Al)

2.2 Identity changes forward chain

w^{ma} denotes the number of kg of material m needed for the manufacturing of 1 kg of component a;

w^{ma}	material m1	material m2	material m3	material m4
a=a1	1	0	0	0
a=a2	0	1	0	0
a=a3	0	0	1	0
a=a4	0	1	0	0
a=a5	1	0	0	0
a=a6	0	1	0	0
a=a7	1	0	0	0
a=a8	0	0	0	1
a=a9	1	0	0	0
a=a10	1	0	0	0
a=a11	1	0	0	0
a=a12	1	0	0	0
a=a13	0	1	0	0
a=a14	1	0	0	0
a=a15	1	0	0	0
a=a16	1	0	0	0
a=a17	1	0	0	0
a=a18	1	0	0	0
a=a19	0	1	0	0
a=a20	0	1	0	0
a=a21	0	1	0	0
a=a22	1	0	0	0
a=a23	0	0	0	1
a=a24	0	1	0	0
a=a25	0	0	0	1

w^{ao} is the amount of kg. of component a needed to assemble 1 kg. of product o. These components are non modular and directly built in

w^{ao}	o=o1	o=o2	o=o3
a1	0	0	0
a2	0	0.32	0
a3	0	0	0.003
a4	0	0.01	0
a5	0	0	0
a6	0	0.01	0
a7	0	0.003	0
a8	0	0	0
a9	0	0	0
a10	0	0.10	0
a11	0	0.01	0
a12	0	0.03	0
a13	0	0.008	0
a14	0	0	0
a15	0	0.003	0
a16	0	0.008	0
a17	0	0	0
a18	0	0.02	0
a19	0	0	0.001
a20	0	0	0
a21	0	0	0.03
a22	0	0.02	0
a23	0	0	0
a24	0	0.02	0
a25	0	0	0

w^{to} is the amount of kg. of module t needed to assemble 1 kg. of product o.

w^{to}	o=o1	o=o2	o=o3
t1	0.86	0	0
t2	0.14	0	0
t3	0	0.04	0
t4	0	0.004	0
t5	0	0.006	0
t6	0	0.02	0
t7	0	0.28	0
t8	0	0.07	0
t9	0	0	0.03
t10	0	0	0.34
t11	0	0	0.006
t12	0	0	0.55
t13	0	0	0.04

2.3 Identity changes in the return part

u_{cp} is the fraction of return flow o feasible for $p5$ (repair) and disassembly ($p6$) depending on return quality. These values are the same for all product types $o=o1..o3$

U_{cp}	$p=p5$	$p=p6$
C1	0.2	1
C2	0.3	1
C3	0.1	1
C4	0.5	1
C5	0.6	1
C6	0.4	1
C7	0.1	1
C8	0	1
C9	1	1
C10	0.85	1

	$p=p8$	$p=p6$	$p=p2$
u_p^t	0.5	1	0.2

fraction of released modules t feasible for $p8$ (rebuilt), $p6$ (further disassembly into components) and $p2$ (direct reuse, available in stock). This is due to quality reasons. These values are the same for all t .

U_p^a is the fraction of released components a feasible for $p2$ (direct reuse), $p9$ (material recycling), $d1..d5$ (thermal recycling) or landfill ($d6$). Feasibility here depends on return quality, material composition, energetic value and legislation. These values are the same for all a .

U_p^a	$p=p2$	$p=p9$	u_d^a	$d=d1..d5$	$d=d6..d10$
A1	1	1	0	0	0
A2	0	0	1	0	0
A3	1	1	0	0	0
a4	0	0	1	0	0
a5	1	1	0	0	0
a6	1	0	1	0	0
a7	1	1	0	0	0
a8	1	1	0	0	0
a9	1	1	0	0	0
a10	1	1	0	0	0
a11	1	1	0	0	0
a12	1	1	0	0	0
a13	1	1	0	0	0
a14	1	1	0	0	0
a15	1	1	0	0	0
a16	1	1	0	0	0
a17	1	1	0	0	0
a18	1	1	0	0	0
a19	0	0	0	1	0
a20	0	0	1	0	0
a21	0	0	0	1	0
a22	1	0	0	1	0
a23	1	1	0	0	0
a24	0	0	1	0	0
a25	1	1	0	0	0

$$r^{ot} = w^{to}$$

$$r^{ta} = w_1^{at}$$

$$r^{am} = w^{ma}$$

note: the reverse BOM is assumed to be the inverse assembly BOM!

2.4 Cost parameters

$$T_{\text{cost}} = 0$$

$$T_{e1} = 0$$

$$T_{e2} = 0$$

$c_{\text{sf}}^m = (\text{manufacturing price} + d(s,f) \cdot 0.005)$ yen per kg.

For distances see distance matrix [kk.xls], $s=s1..s10$, $f=f1..f20$

manufacturing prices are:

m1: 100 yen/kg

m2: 200 yen/kg

m3: 1000 yen/kg

m4: 1500 yen/kg

in case material m cannot be supplied from s, costs are set infinite, transportation per ship incurs half the variables transportation costs

$c_{\text{ff}} = d(f,f') \cdot 0.005$ yen per kg. $f=f1..f20$, $f'=f1..f20$, see distance matrix.

$c_{\text{fc}} = d(f,d) \cdot 0.005$ yen per kg. $f=f1..f20$ $c=c1..c10$

$c_{\text{fd}}^a = \text{disposal/thermal recycling tariff} + d(f,d) \cdot 0.005$ yen per kg. in case disposal is allowed else infinite

disposal tariff yen/kg	d1..d5 (thermal)	d6..d10 (disposal)
a2	100	∞
a4	100	∞
a6	100	∞
a13	100	∞
a19	∞	150
a20	100	∞
a21	∞	150
a22	∞	150
a24	100	∞

for all other a c_{fd}^a is infinite for all d

$c_{\text{pf}}^a = \text{yen/kg}$

c_{pf}^a	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	a11	a12	a13
p1	112	415	930	632	851	1077	1152	1401	433	150	683	239	438
p2	10	10	10	10	10	10	10	10	10	10	10	10	10
p7	4	3.4	30	100	200	110	500	200	100	12	100	40	180
p9	75	∞	750	∞	75	∞	75	750	75	75	75	75	∞
c_{pf}^a	a14	a15	a16	a17	a18	a19	a20	a21	a22	a23	a24	a25	
p1	343	367	536	214	214	2465	350	758	2033	6720	1192	2000	
p2	10	10	10	10	10	10	10	10	10	10	10	10	
p7	80	40	142	55	56	1000	149	33	67	900	71	1000	
p9	75	75	75	75	75	∞	∞	∞	∞	750	∞	750	

for other p costs are infinite. values are the same for all f, except for locations in Ireland and Eastern Europe which are 25% cheaper

c_{pf}^t in yen/kg

c_{pf}^t	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13
p2	10	10	10	10	10	10	10	10	10	10	10	10	10
p3	50	84	111	1000	667	181	16	59	154	13	667	41	324
p6	50	84	111	1000	667	181	16	59	154	13	667	41	324
p7	2.5	16.8	55.5	500	333	90.9	7.8	29.4	77	6.5	333	4	54
p8	50	84	111	1000	667	181	16	59	154	13	667	41	324

for other processes p costs are infinite. values are the same for all f, except for locations in Ireland and Eastern Europe which are 25% cheaper

c_{pf}^o in yen/kg

	p2	p4	p5	p6
o1	10	2	2000	2
o2	10	21	1500	21
o3	10	9	1750	9

for other processes p costs are infinite, values are the same for all f, except for locations in Ireland and Eastern Europe which are 25% cheaper

FIX_{pf} in 1000 yen

p1	p2	p3	p4	p5	p6	p7	p8	p9
34176	20000	5000	5000	1000	5000	100	500	3800

values are the same for all f

Energy costs are expressed in J/kg good flow (m,a,t,o) and calculated as follows:

$c(e1)_{sf}^m$ is calculated as (supply energy per material m)+(distance(s,f)*0.85J/kg/km)

use distancematrix km value times 0.85 MJ per ton, in case of ship transportation the energy times is 0.2 MJ per ton

Supply energy per material m (1 kwh = $3.6 \cdot 10^6$ J),

	kwh/kg	J/kg
M1	14.7	52.9 10E6
M2	0.5	1.8 10E6
M3	4.1	14.8 10E6
M4	21.1	75.9 10E6

$c(e1)_{ff}$ is calculated as distance(f,f)*0.85J/kg/km, see distance matrix, distance in km

$c(e1)_{fc}$ is calculated as distance(f,c)*0.85 J/kg/km, see distance matrix, distance in km

$c(e1)_{fd}^a$ is calculated as (distance(f,d)*0.85 J/ kg/km) + (energy values of the disposal sink process d for each a)

Values of thermal recycling and disposal process in kwh/kg.

	d1..d5		d6..d10	
	Kwh/kg	J/kg	Kwh/kg	J/kg
a1	∞	∞	∞	∞
a2	-0.084	-302400	∞	∞
a3	∞	∞	∞	∞
a4	-0.084	-302400	∞	∞
a5	∞	∞	∞	∞
a6	-0.084	-302400	∞	∞
a7	∞	∞	∞	∞
a8	∞	∞	∞	∞
a9	∞	∞	∞	∞
a10	∞	∞	∞	∞
a11	∞	∞	∞	∞
a12	∞	∞	∞	∞
a13	-0.084	-302400	∞	∞
a14	∞	∞	∞	∞
a15	∞	∞	∞	∞
a16	∞	∞	∞	∞
a17	∞	∞	∞	∞
a18	∞	∞	∞	∞
a19	∞	∞	0.025	90000
a20	-0.084	-302400	∞	∞
a21	∞	∞	0.025	90000
a22	∞	∞	0.025	90000
a23	∞	∞	∞	∞
a24	-0.084	-302400	∞	∞
a25	∞	∞	∞	∞

$c(e1)_{pf}^a$ in J/kg

	a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	a11	a12	a13	a14	a15	a16	a17	a18	a19	a20	a21	a22	a23	a24	a25
p1	10.8E6	18E6	11.9E6	18.7E6	10.8E6	18E6	10.8E6	11.5E6	10.8E6	10.8E6	10.8E6	11.5E6	19.1E6	11.5 E6	11.5 E6	12.6E6	11.2 E6	11.2E6	18E6	18E6	18E6	2.5E6	12.6E6	11.2E6	10.8E6
p2	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400
p7	14400	144000	108000	36000	108000	36000	180000	72000	36000	3600	36000	14400	72000	36000	14400	72000	18000	18000	360000	7200	10800	25200	360000	25200	360000
p9	52.9E6	10E40	14.8E6	10E40	52.9E6	10E40	52.9E6	36E6	52.9E6	52.9E6	52.9E6	52.9E6	10E40	52.9E6	52.9E6	52.9E6	52.9E6	52.9E6	10E40	10E40	10E40	10E40	36E6	10E40	14.8E6

for other processes p set energy use infinite. costs are the same for all f

$c(e1)_{pf}^f$ in J/kg

c_{pf}^f	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13
p2	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400	14400
p3	72000	108000	144000	1.26E6	828000	216000	18000	72000	180000	18000	828000	108000	396000
p6	72000	108000	144000	1.26E6	828000	216000	18000	72000	180000	18000	828000	108000	396000
p7	360	28800	10800	108000	72000	18000	1440	3600	14400	1080	72000	720	10800
p8	108000	144000	180000	1.6E6	1.15E6	288000	32400	108000	252000	3240	1.18E6	144000	540000

for other processes, energy use are infinite. costs are the same for all f.

$c^o(e1)_{pf}$ in J/kg

c_{pf}^o	p2	p4	p5	p6
o1	14400	7200	1.8E6	7200
o2	14400	72000	1.1E6	72000
o3	14000	25200	720000	25200

for other processes, energy use are infinite. costs are the same for all f.

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